


Table 5-8 (continued)											
$F_y = 50$ ksi $F_u = 65$ ksi						Available Strength in Axial Tension					
Double Angles						 2L5-2L3					
Shape	Gross Area, $A_g$	Yielding		Rupture, $A_e = 0.75A_g$		Shape	Gross Area, $A_g$	Yielding		Rupture, $A_e = 0.75A_g$	
		kips		kips				kips		kips	
		$P_n / \Omega_t$	$\phi_t P_n$	$P_n / \Omega_t$	$\phi_t P_n$			$P_n / \Omega_t$	$\phi_t P_n$	$P_n / \Omega_t$	$\phi_t P_n$
		in. <sup>2</sup>	ASD	LRFD	ASD			LRFD	in. <sup>2</sup>	ASD	LRFD
2L5×3½×¾	11.7	350	527	285	428	2L3½×3½×½	6.50	195	293	159	238
×¾	9.86	295	444	241	361	×¾	5.78	173	260	141	212
×½	8.00	240	360	195	293	×¾	5.00	150	225	122	183
×¾	6.10	183	275	149	223	×¾	4.20	126	189	102	154
×¾	5.12	153	230	125	187	×¼	3.40	102	153	82.9	124
×¼	4.14	124	186	101	152						
2L5×3×½	7.50	225	338	183	274	2L3½×3×½	6.04	181	272	147	221
×¾	6.62	198	298	162	242	×¾	5.34	160	240	130	195
×¾	5.72	171	257	139	209	×¾	4.64	139	209	113	170
×¾	4.82	144	217	118	176	×¾	3.90	117	176	95.2	143
×¼	3.88	116	175	94.6	142	×¼	3.16	94.6	142	77.0	116
2L4×4×¾	10.9	326	491	266	399	2L3½×2½×½	5.54	166	249	135	203
×¾	9.22	276	415	225	337	×¾	4.24	127	191	103	155
×½	7.50	225	338	183	274	×¾	3.58	107	161	87.4	131
×¾	6.60	198	297	161	241	×¼	2.90	86.8	131	70.9	106
×¾	5.72	171	257	139	209	2L3×3×½	5.52	165	248	135	202
×¾	4.80	144	216	117	176	×¾	4.86	146	219	119	178
×¼	3.86	116	174	94.3	141	×¾	4.22	126	190	103	155
2L4×3½×½	7.00	210	315	171	256	×¾	3.56	107	160	86.8	130
×¾	5.36	160	241	131	196	×¼	2.88	86.2	130	70.2	105
×¾	4.50	135	203	110	165	×¾	2.18	65.3	98.1	53.3	80.0
×¼	3.64	109	164	88.7	133	2L3×2½×½	5.00	150	225	122	183
2L4×3×¾	7.98	239	359	195	292	×¾	4.44	133	200	108	162
×½	6.50	195	293	159	238	×¾	3.86	116	174	94.3	141
×¾	4.98	149	224	122	182	×¾	3.26	97.6	147	79.6	119
×¾	4.18	125	188	102	153	×¼	2.64	79.0	119	64.4	96.5
×¼	3.38	101	152	82.6	124	×¾	2.00	59.9	90.0	48.8	73.1
						2L3×2×½	4.52	135	203	110	165
						×¾	3.50	105	158	85.5	128
						×¾	2.96	88.6	133	72.2	108
						×¼	2.40	71.9	108	58.5	87.8
						×¾	1.83	54.8	82.4	44.5	66.8
Limit State	ASD	LRFD		Note: Tensile rupture on the effective net area will control over tensile yielding on the gross area unless the tension member is selected so that an end connection can be configured with $A_e \geq 0.923A_g$ .							
Yielding	$\Omega_t = 1.67$	$\phi_t = 0.90$									
Rupture	$\Omega_t = 2.00$	$\phi_t = 0.75$									